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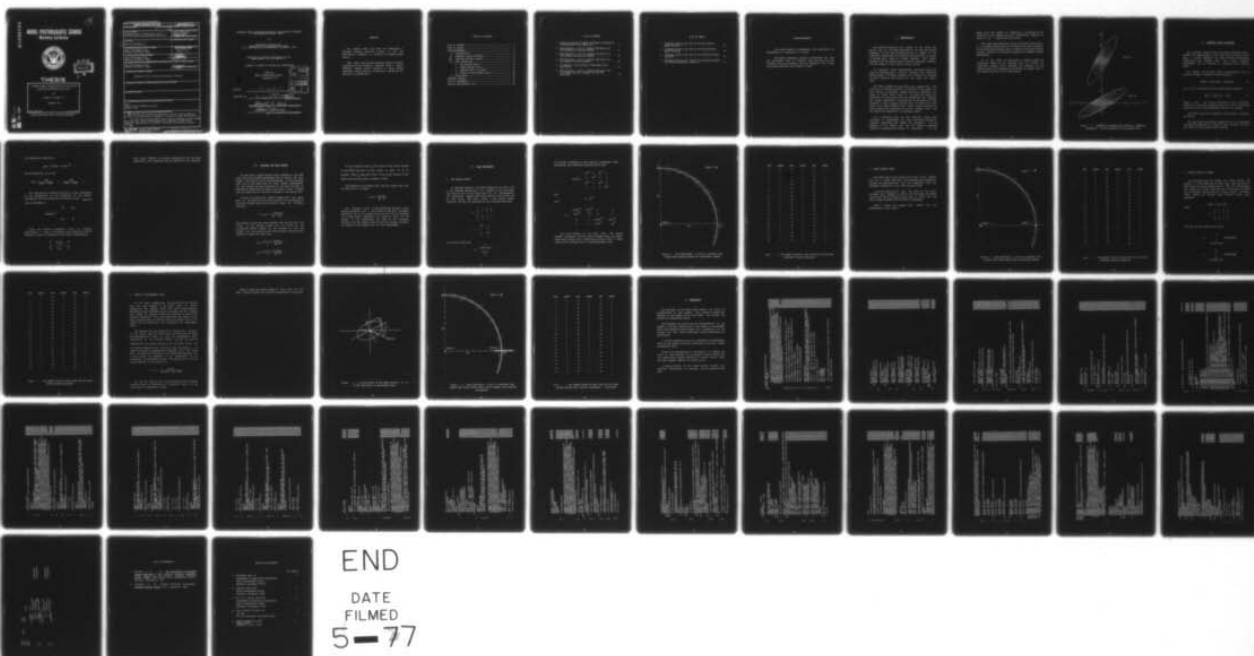
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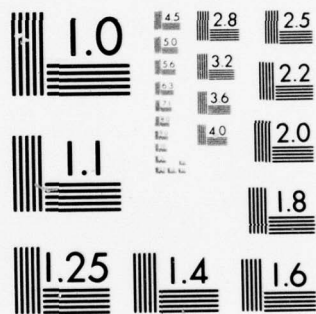
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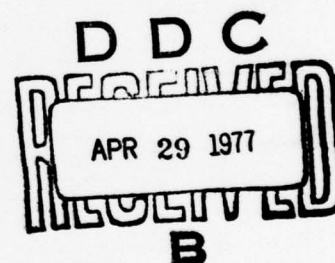
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NAVAL POSTGRADUATE SCHOOL

Monterey, California



THESIS

EXTENDED KALMAN FILTERING APPLIED TO THE POSITION
LOCATING AND REPORTING SYSTEM (PLRS)

by

Bernard M. de Mahy, Jr.

December 1976

Thesis Advisor:

H. A. Titus

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EXTENDED KALMAN FILTERING APPLIED TO THE POSITION LOCATING
AND REPORTING SYSTEM (PLRS)

by

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Captain, United States Marine Corps
B.S., University of Southwestern Louisiana, 1969

Submitted in partial fulfillment of the
requirements for the degree of

MASTER OF SCIENCE IN ELECTRICAL ENGINEERING

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Dean of Science and Engineering

ABSTRACT

The Marine Corps and Army are developing a Position Locating Reporting System to aid the battlefield commander in locating his assets during battle.

This study has applied Extended Kalman Filtering techniques to that problem, evolving from a simple Extended Kalman Filter Observer to three moving observers, whose position is uncertain, estimating the position of another unit.

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I. INTRODUCTION

The precise location of all assets in and about the battle area is of prime importance to the tactical Marine Commander. In the past locating has had to depend on the individual knowing his own position and being able to report it through radio links to higher command. This system suffered from the limitations of terrain, daylight, weather, and the volume of radio traffic during battle.

To alleviate these shortcomings the Marine Corps and Army are investigating a Position Locating and Reporting System (PLRS) to collect, process, and, display the location of units, vehicles, and aircraft in and about the battle area.

The PLRS consists of field units and a master unit. The field unit is compact enough to be carried in the field by a man, vehicle, or aircraft. These units will determine the range to other field units in the area and report this information to the master unit for processing and display. The range information is determined by measuring the time required to send a signal from one unit to another and back again plus some "system" delay. When a unit's position is being updated it is referred to as the "Update" unit; and all others are referred to as "Ranging" units.

In a previous study in this area,[1], tests were conducted to investigate the use of the error ellipse in visually displaying the degree of uncertainty of the position of an update unit and the effect of numerous updates on reducing that degree of uncertainty. It was

found that the degree of uncertainty is reduced in the direction of the ranging unit with consecutive updates as shown in Fig 1 taken from that study.

That study also simulated one jet aircraft flying Mach 1 in a constant radius turn as an update unit being ranged on by two stationary ranging units to explore the proper random forcing excitation covariance necessary for adequate filter performance.

It is the intent of this study to further expand the simulation begun in the previous work by adding an additional ranging unit, allowing the movement of the ranging units, and considering the effect of ranging from a unit whose position is not known exactly

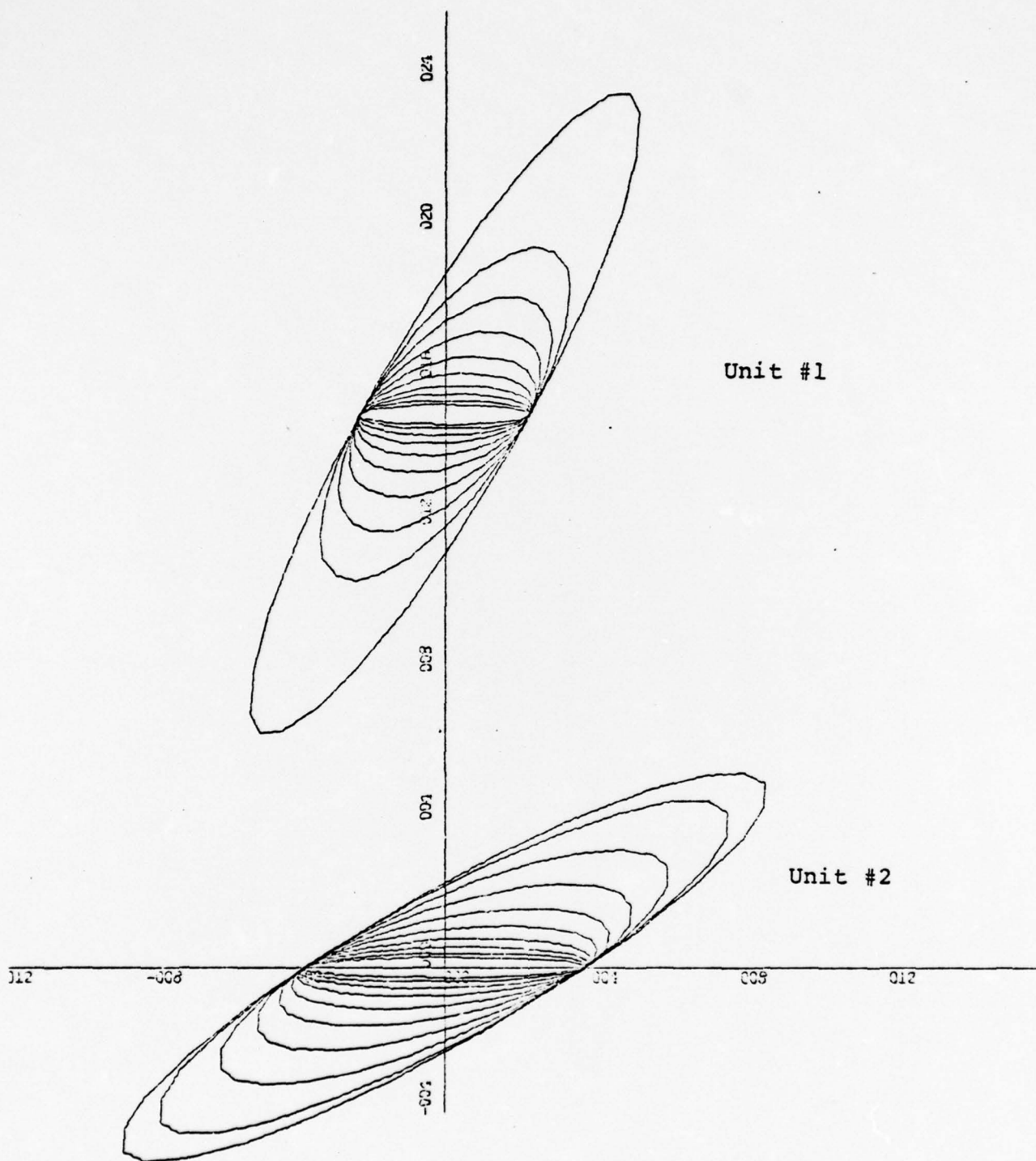


Figure 1 - CONSECUTIVE UPDATES WILL REDUCE THE DEGREE OF
UNCERTAINTY IN THE DIRECTION OF THE RANGING UNIT

II. EXTENDED KALMAN FILTERING

The Extended Kalman Filter is widely documented and no attempt at a development of that theory will be made in this work. A brief treatment has been included to establish nomenclature and formulas used. For a more complete development one is referred to reference [2] or similar texts.

As defined in this work, PLRS is described by a set of discrete, linear, cartesian system equations

$$\underline{x}(k+1) = \underline{\phi}(k) \underline{x}(k) + \underline{\Gamma}(k) \underline{w}(k) \quad (1)$$

and a set of discrete non-linear measurement equations

$$\underline{z}(k) = \underline{m}(\underline{x}(k), k) + \underline{v}(k) \quad (2)$$

where $\underline{\phi}$ and $\underline{\Gamma}$ are linear functions and \underline{m} is a nonlinear function of the state variables $\underline{x}(k)$; $\underline{w}(k)$ is the excitation noise and $\underline{v}(k)$ is the measurement noise of the system.

The plant noises are considered uncorrelated, zero-mean, and white.

The non-linear measurement equations can be linearized by expanding equation (2) around the best estimate at time k and using the first-order terms yielding

$$\underline{z}(k) = \underline{H}(k) \underline{x}(k) + \underline{v}(k)$$

where

$$H(k) = \frac{\partial m}{\partial \underline{x}} \underline{x} = \underline{\hat{x}}(k/k-1) \quad (3)$$

$\underline{\hat{x}}(k/k)$ is the estimated value of the state at k after the k^{th} measurement and $\underline{\hat{x}}(k/k-1)$ is the predicted value of the state at time k before the k^{th} measurement.

The state error vector is

$$\underline{\hat{x}}'(k/k) = \underline{\hat{x}}(k/k) - \underline{\hat{x}}(k)$$

and the predicted error vector is

$$\underline{\hat{x}}'(k/k-1) = \underline{\hat{x}}(k/k-1) - \underline{x}(k)$$

The covariance of the state error matrix is

$$P(k/k) = E[\underline{\hat{x}}'(k/k) \underline{\hat{x}}'^T(k/k)]$$

and the predicted covariance of the state error matrix is

$$P(k/k-1) = E[\underline{\hat{x}}'(k/k-1) \underline{\hat{x}}'^T(k/k-1)] .$$

The state excitation matrix is

$$Q(k) = E[\underline{\Gamma}(k) \underline{w}(k) \underline{w}^T(k) \underline{\Gamma}^T(k)]$$

and the measurement noise covariance matrix is

$$R(k) = E[\underline{v}(k) \underline{v}^T(k)] .$$

The equations that made up the Kalman Filter used in this work are as follows:

$$P(k/k-1) = \underline{\Phi}(k) P(k/k) \underline{\Phi}^T(k) + Q(k)$$

$$G(k) = P(k/k-1) \underline{H}^T(k) [\underline{H}(k) P(k/k-1) \underline{H}^T(k) + R(k)]^{-1}$$

$$P(k/k) = [I - G(k) \underline{H}(k)] P(k/k-1)$$

$$\hat{\underline{x}}(k/k) = \hat{\underline{x}}(k/k-1) + G(k) [\underline{z}(k) - \underline{H}(k) \hat{\underline{x}}(k/k-1)]$$

$$\hat{\underline{x}}(k/k-1) = \underline{\Phi}(k) \hat{\underline{x}}(k/k)$$

$$\underline{z}(k) = \underline{m}(\underline{x}(k/k-1), k)$$

Since the only observations in this system are ranges,

the observation equation is

$$\underline{z}(k) = [x^2(k) + y^2(k)]^{1/2} ;$$

and from equation (3) we get

$$H(k) = \frac{x(k)}{x^2(k) + y^2(k)} \quad 0 \quad \frac{y(k)}{x^2(k) + y^2(k)} \quad 0 .$$

The covariance of estimation error, P , is an expression of the uncertainty in the estimation of the states. Considering only the estimation's position error, P_{position} can be expressed as

$$P_{\text{position}} = \begin{bmatrix} \sigma_x^2 & \sigma_x \sigma_y \\ \sigma_y \sigma_x & \sigma_y^2 \end{bmatrix}$$

Since the position estimation error is normally distributed, a curve of constant error probability can be defined by using the exponent of the normal distribution,

$$\frac{x^2}{\sigma_x^2} - \frac{2r_{xy} xy}{\sigma_x \sigma_y} + \frac{y^2}{\sigma_y^2}$$

This curve defines an ellipse. Graphically, for the given probability, the estimation may be anywhere in that ellipse.

III. CHOOSING THE BEST RANGER

To move from a simple Kalman Filter observer to the PLRS model the first problem encountered was to choose the best ranger from which to take the measurement. In the previous work [1], it was shown that the most useful measurement, the one causing the most reduction in the error ellipse, is obtained by observing the update unit from a point aligned with the major axis of the error ellipse of the update unit.

To find the ranger most closely aligned with the major axis of the update unit's error ellipse the orientation of the error ellipse must first be found using the following equation.

$$\theta = \frac{1}{2} \tan^{-1} \frac{2 \text{Cov}(x,y)}{\sigma_x^2 - \sigma_y^2}$$

This angle(θ) gives the angle between -90° and 90° that the x-axis of the ellipse makes with the x-axis of the co-ordinate system. Looking at the ellipse in this new posture one can find the new "Uncorrelated" variances that define the major and minor axes.

$$\sigma_{x'}^2 = \frac{\sigma_x^2 + \sigma_y^2}{2} + \frac{\text{Cov}(x,y)}{\sin 2\theta} ,$$

$$\sigma_{y'}^2 = \frac{\sigma_x^2 + \sigma_y^2}{2} - \frac{\text{Cov}(x,y)}{\sin 2\theta} ,$$

If σ_x^2 is greater than σ_y^2 the x-axis of the error ellipse is the major axis and θ is the angle we seek. If σ_y^2 is greater than σ_x^2 then the y-axis of the error ellipse is the major axis and the angle we seek is $\theta + 90^\circ$.

The bearing of the update unit from the ranger must then be found and it is simply

$$\beta = \text{Tan}^{-1} \frac{Y_u - Y_R}{X_u - X_R}.$$

The absolute value of the difference between θ , after proper correction, and β was chosen as the best alignment indicator; but to be aligned and to be 180° out of alignment is of equal value; therefore the absolute value of the cosine of the differences was used as the alignment indicator and the ranger found to have the largest indicator was chosen as the ranging unit for that measurement.

IV. PLRS SIMULATION

A. TWO RANGING UNITS

In previous work,[1], the PLRS simulation was setup for a jet aircraft flying Mach 1 in a constant 10 Km turn about the origin to act as the update unit for all measurements. Two stationary ranging units were placed at the origin and at 10Km north, 10Km east. Using a one second sample interval, the jet was described by the following matrices:

$$\phi = \begin{array}{cccc} 1 & 1 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 1 \\ 0 & 0 & 0 & 1 \end{array}$$

$$\Gamma = \begin{array}{cc} 0.5 & 0 \\ 1 & 0 \\ 0 & 0.5 \\ 0 & 1 \end{array}$$

Its initial state was

$$\underline{x} = \begin{array}{c} 0 \\ 0.333 \text{ Km/s} \\ 10 \text{ Km} \\ 0 \end{array}$$

Its initial covariance of error matrix, measurement noise covariance, and excitation forcing matrix were

$$P(1/0) = \begin{bmatrix} 10^{-4} & 0 & 10^{-4} & 0 \\ 0 & 10^{-4} & 0 & 0 \\ 10^{-4} & 0 & 10^{-4} & 0 \\ 0 & 0 & 0 & 10^{-4} \end{bmatrix}$$

and

$$R = 10^{-4}$$

with

$$Q = \begin{bmatrix} 2.5 \times 10^{-5} & 5 \times 10^{-5} & 0 & 0 \\ 5 \times 10^{-5} & 10^{-4} & 0 & 0 \\ 0 & 0 & 2.5 \times 10^{-5} & 5 \times 10^{-5} \\ 0 & 0 & 5 \times 10^{-5} & 10^{-4} \end{bmatrix}$$

Fig 2 is a display of its final runs. The filter tracked accurately and the error ellipses shown are twenty times their actual size to make them visible. Table 1 shows which was the ranging unit at each measurement time.

TIME	RANGER	TIME	RANGER	TIME	RANGER
1	2	21	2	41	1
2	1	22	1	42	2
3	2	23	2	43	1
4	1	24	1	44	2
5	2	25	1	45	1
6	1	26	2	46	2
7	2	27	1	47	1
8	1	28	2	48	2
9	2	29	1	49	1
10	1	30	2	50	2
11	2	31	1	51	1
12	1	32	2	52	2
13	2	33	1	53	1
14	1	34	2	54	2
15	2	35	1	55	1
16	1	36	2	56	2
17	2	37	1	57	1
18	1	38	2	58	2
19	2	39	1	59	1
20	1	40	2	60	2

TABLE 1 - THE RANGER CHOSEN AT EACH TIME FOR THE PLRS TWO
STATIONARY RANGER SIMULATION

B. THREE RANGING UNITS

The first step of this study was to add a third ranging unit at 0 north, 10Km east. The algorithm was enlarged to include the additional unit and its comparison with the alignment indicators of the other ranging units.

It can be seen in Fig 3 that the size of the error ellipses were reduced in size in the mid-range area where the jet and the two original units were in line; and the third ranger provides the triangular measurement.

Table 2 shows the ranging unit chosen for the measurement at each time k.

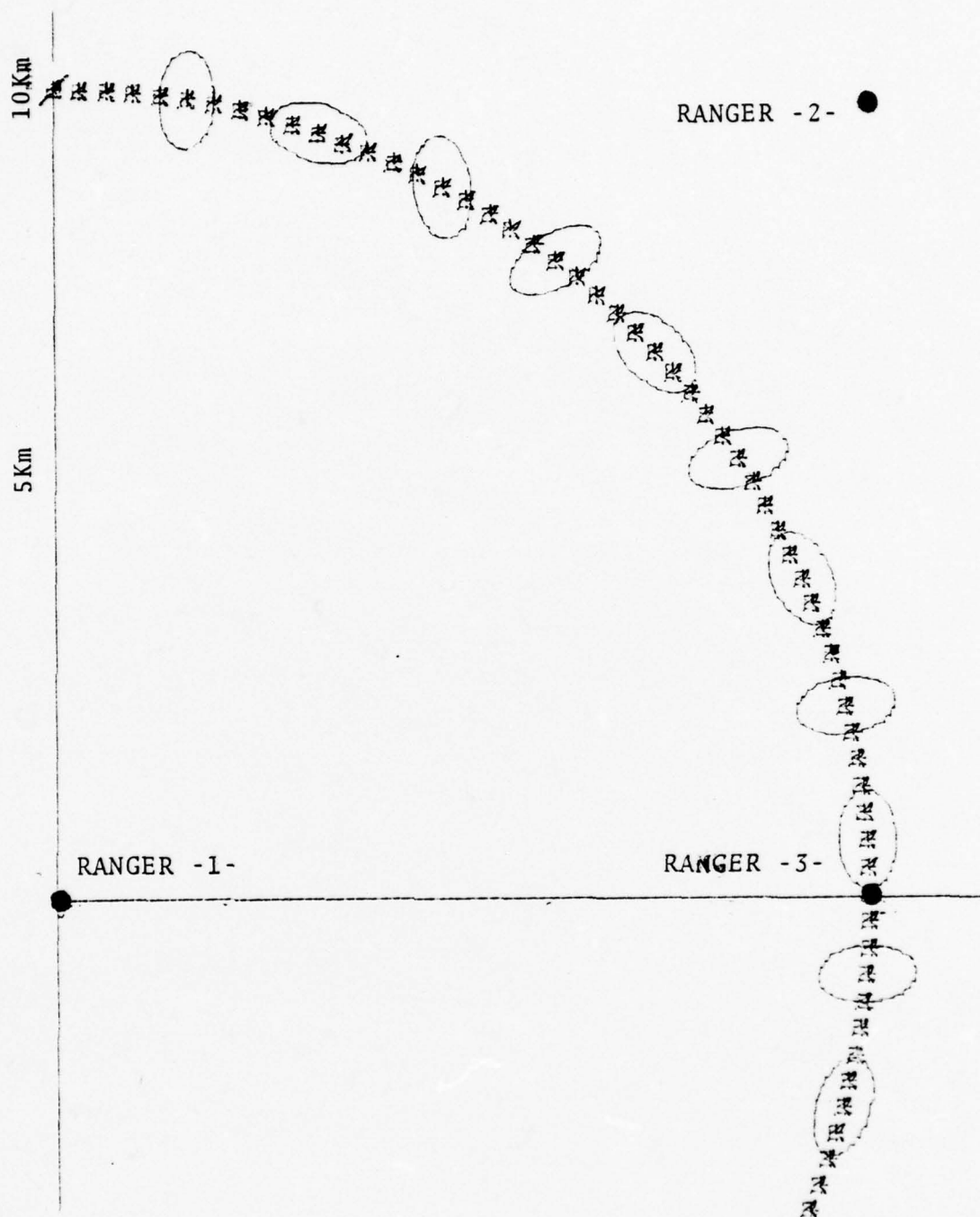


Figure 3 - PLRS SIMULATION - A JET IN A CONSTANT 10KM
RADIUS TURN FLYING AMONG THREE STATIONARY RANGERS

TIME	RANGER	TIME	RANGER	TIME	RANGER
1	2	21	2	41	1
2	1	22	3	42	3
3	2	23	2	43	1
4	1	24	3	44	3
5	2	25	1	45	1
6	1	26	3	46	3
7	2	27	1	47	1
8	1	28	3	48	2
9	2	29	1	49	1
10	1	30	3	50	2
11	2	31	1	51	1
12	1	32	3	52	3
13	2	33	1	53	1
14	3	34	3	54	3
15	2	35	1	55	1
16	3	36	3	56	3
17	2	37	1	57	1
18	3	38	3	58	3
19	2	39	1	59	1
20	3	40	3	60	3

TABLE 2 - THE RANGER CHOSEN AT EACH TIME FOR THE THREE
STATIONARY RANGER SIMULATION

C. RANGING UNITS IN MOTION

In the second step the rangers are given motion. The rangers at the origin and at 10Km north, 10Km east were to move north and south respectively at 3Kts as infantrymen. The ranger at 0 north, 10Km east was to move west at 120Kts as a helicopter. Again using one second sample intervals, their motion was defined using discrete linear state equations

$$x(k+1) = \phi(k) x(k) ,$$

where

$$\phi = \begin{bmatrix} 1 & 1 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

with the initial states shown below;

$$x = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 1.67 \times 10^3 \text{ Km/s} \end{bmatrix} \quad \text{INFANTRYMAN}$$

$$x = \begin{bmatrix} 10 \\ 0 \\ 10 \\ -1.67 \times 10^3 \text{ Km/s} \end{bmatrix} \quad \text{INFANTRYMAN}$$

$$\begin{array}{rcl}
 & 12 & \\
 x = & -5.555 \times 10^2 & \text{Km/s} \quad \text{HELICOPTER} \\
 & 0 & \\
 & 0 &
 \end{array}$$

It can be seen in Fig 4 that no system depreciation resulted from the motion of the rangers, Table 3 shows the ranging unit chosen for the measurement at each time,

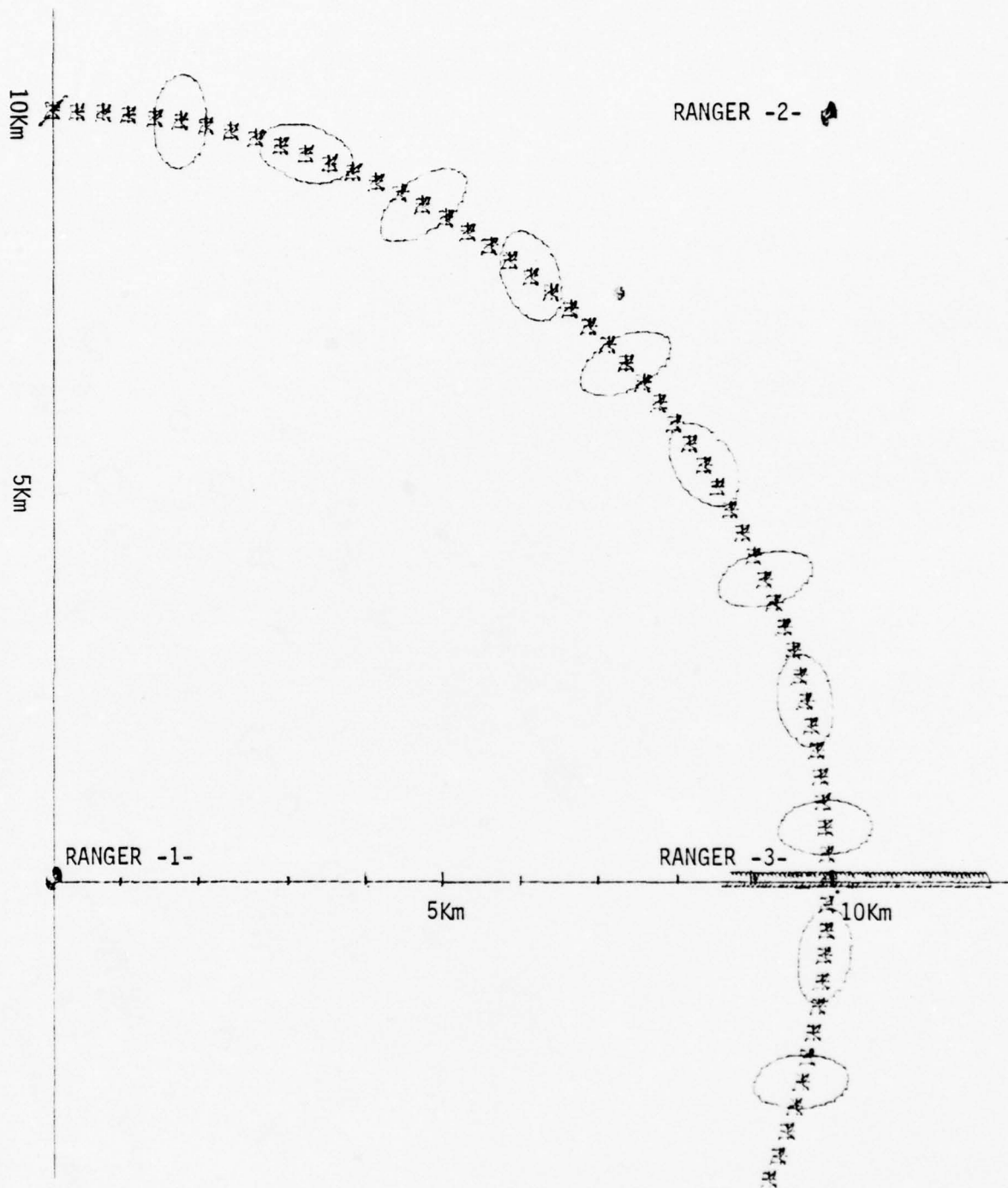


Figure 4 - PLRS SIMULATION - A JET IN A CONSTANT 10KM
RADIUS TURN FLYING AMONG THREE MOVING RANGERS

TIME	RANGER	TIME	RANGER	TIME	RANGER
1	2	21	3	41	3
2	1	22	2	42	1
3	2	23	3	43	2
4	1	24	2	44	1
5	2	25	3	45	2
6	1	26	1	46	1
7	2	27	3	47	2
8	1	28	1	48	1
9	2	29	3	49	2
10	1	30	1	50	1
11	2	31	3	51	2
12	1	32	1	52	1
13	3	33	3	53	2
14	1	34	1	54	1
15	3	35	3	55	2
16	2	36	1	56	1
17	3	37	3	57	2
18	2	38	1	58	1
19	3	39	3	59	2
20	2	40	1	60	1

TABLE 3 - THE RANGER CHOSEN AT EACH TIME FOR THE THREE
MOVING RANGER SIMULATION

D. SOURCE OF MEASUREMENT NOISE

In the above simulations the position of the ranging unit has been assumed to be exact; while in actual application the ranging units will have covariances of estimation error defining an error ellipse; and the ranging unit might be anywhere within that ellipse. To bring this position uncertainty into the simulation, the radius of the error ellipse along the bearing from the ranging unit to the update unit was defined as the covariance of measurement error.

The equation for the radius of an ellipse is a function of the major axis, the minor axis, and the angle at which the measurement is made. To find the measurement noise covariance, or the ellipse radius, σ_x^2 and σ_y^2 must be compared and the larger defined as M_j , the major axis, and the smaller defined as M_n , the minor axis. The angle, α , at which the radius is determined is measured from the major axis and thus is calculated as the difference between θ and β . Fig 5 shows the geometry of the calculation of the covariance of measurement noise. The equation for R and the radius squared of the ellipse is:

$$R = r^2 = \frac{M_j M_n}{M_j \sin^2 \alpha + M_n \cos^2 \alpha}$$

It can be seen in Fig 6 that performance was improved slightly using the covariance of estimation error as the sole source of measurement noise.

Table 4 shows the ranger chosen at each time for the three moving rangers with position uncertainty simulation.

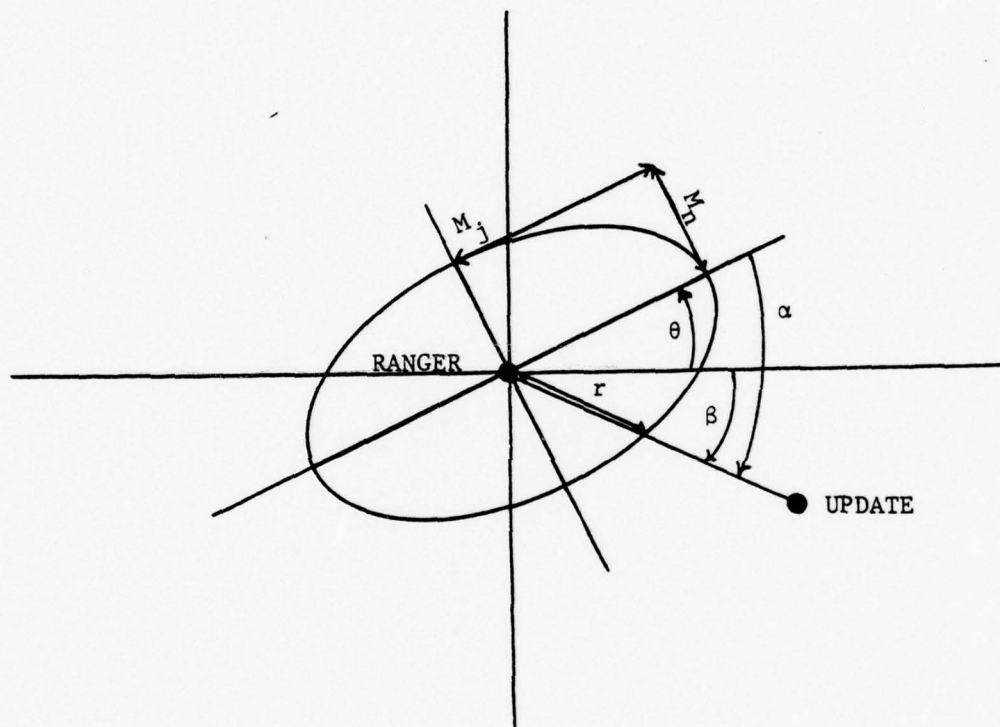


Figure 5 - r IS THE RADIUS OF THE ERROR ELLIPSE - $r^2 = R$
IS THE COVARIANCE OF MEASUREMENT NOISE

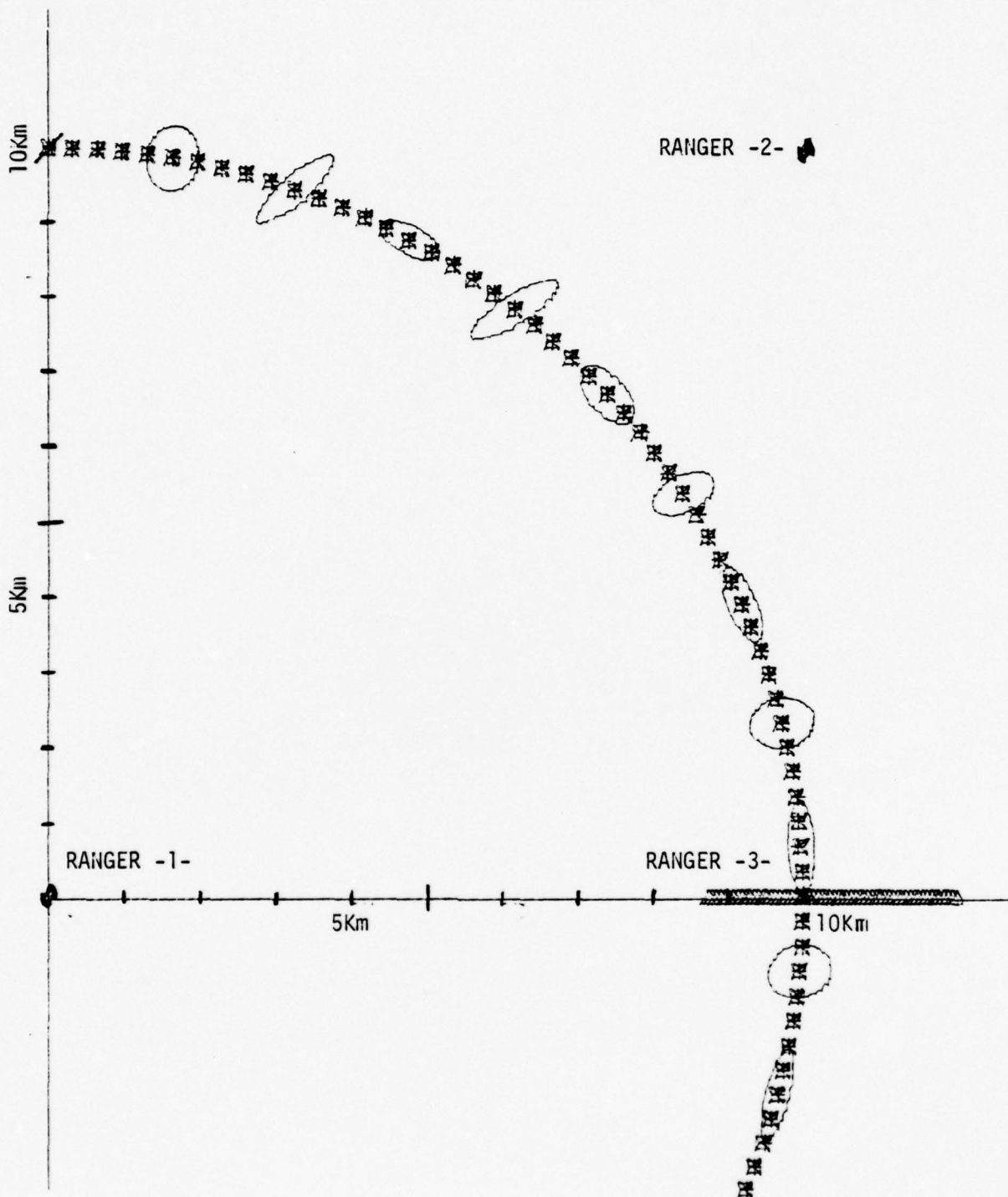


Figure 6 - PLRS SIMULATION - A JET IN A CONSTANT 10KM
RADIUS TURN FLYING AMONG THREE MOVING RANGERS WITH POSITION
UNCERTAINTY

TIME	RANGER	TIME	RANGER	TIME	RANGER
1	2	21	2	41	1
2	1	22	3	42	2
3	2	23	2	43	1
4	1	24	3	44	2
5	2	25	1	45	1
6	1	26	3	46	2
7	2	27	1	47	1
8	1	28	3	48	2
9	2	29	1	49	1
10	3	30	3	50	2
11	1	31	1	51	1
12	3	32	3	52	2
13	1	33	1	53	1
14	3	34	3	54	2
15	1	35	1	55	1
16	3	36	3	56	2
17	1	37	1	57	1
18	3	38	3	58	2
19	2	39	1	59	1
20	3	40	3	60	2

TABLE 4 - THE RANGER CHOSEN AT EACH TIME FOR THE THREE
MOVING RANGERS WITH POSITION UNCERTAINTY SIMULATION

V. CONCLUSION

The placement of the third ranger showed the value of triangulation of the rangers. The closer to normal the bearings of the rangers are to each other, the better the results of consecutive ranges.

The allowance for motion and the representation of the ranger's position uncertainty as the source of measurement error were important steps toward full simulation of the system; and they were accomplished without degradation of performance.

A better simulation may be to represent the measurement error as the ranger's position uncertainty plus some system measurement error.

Still to be accomplished is the ability to update all units at each ranging, and to provide a gating system that will demand more frequent updates for faster moving units and less frequent updates for slower units.

A program listing of the three moving rangers with position uncertainty is included with an annotated data deck.


```

// EXEC FORTCLGP,REGION.G0=200K
//FORT.SYSIN DD *
C      PLRS
C
C      REAL*8 GAMMA,COVM,R,PHI,H,TEMP,TEMP1,PKKM1,G,PKK,Q,EI,PR,PRR
C      COMMON EI(4,4),Q(4,4),G(4,4),PKK(4,4),GAMMA(4,4),COVM(4,4),
C      1TEMP(4,4),TEMP1(4,4),TEMP2(4,4),H(4,4),PKKM1(4,4),PHI(4,4),
C      2VAR(4,4,60),GKS(4,4,60),PKKS(4,4,60),XM(4,4,60),ERR(4,4,60),
C      3GAMMAS(4,4),PHIS(4,4),XS(4,4,60),HS(4,4),GK(4,4),SIGW(4,4),X(4,4),
C      4SIGXZ(4,4),XZMEAN(4,4),XHKKM1(4,4),VTMP(4,4),Z(4,4),V(4,4),SIGV(4,4),
C      5XHATZ(4,4),XZ(60),YZ(60),PX(10),PY(10),PR(4,4,4),
C      6N,NSAM,IQ,M,ITER,ITRK,IN,ISTAT,K,ITRO,IXZ,IV,IW,IEST,ND,NR
C      DIMENSION XP(80),YP(80),PPR(4,4)
C
C      N=ORDER OF SYSTEM MODEL AND FILTER (DIMENSION OF X,XHAT)
C      M=NUMBER OF MEASUREMENTS (DIMENSION OF THE VECTOR Z)
C      IN=NUMBER OF INPUT RANDOM FORCING FCNS (=DIMENSION OF W)
C      NSAM=NUMBER OF TIME SAMPLES
C      NENS=NUMBER OF MEMBERS IN ENSEMBLE
C      READ (5,81) N,M,IN,NSAM,NENS,NR
C
C      READ (5,82) ND
C      THE VALUE OF ND READ IN MUST EQUAL THE ROW (AND COLUMN) DIMENSION
C      SPECIFIED FOR THE SQUARE MATRIX "TEMP1", E.G. IF TEMP1(3,3) IS
C      SPECIFIED IN THE COMMON STATEMENT "ND" MUST BE EQUAL TO 3.
C
C      IPRT=0 -- SOME OR ALL OUTPUT DATA IS PRINTED
C      IPLT=0 -- SOME OR ALL OUTPUT DATA IS PLOTTED
C      READ (5,84) IPRT,IPLT
C
C      CALL OVFLOW
C      IW = 6395217
C      IV = 1936748
C      IXZ = 135769
C
C      THE FOLLOWING SECTION READS THE SPECIFIED INPUT MATRICES
C      CALL MREAD (PHI,N,N)

```

```

MCSP00006
CH3*****
MCSP00008
MCSP00009
CH2000002
CH2000003
MCSP00012
CH2000004
CH2*****
MCSP00016
MCSP00017
MCSP00018
MCSP00019
MCSP00020
MCSP00021
MCSP00022
MCSP00023
MCSP00024
MCSP00025
MCSP00026
MCSP00027
CH2000005
MCSP00029
MCSP00030
MCSP00031
MCSP00032
MCSP00033
MCSP00034
MCSP00068
MCSP00069
MCSP00070
MCSP00071
MCSP00073
MCSP00072
MCSP00035
MCSP0108
MCSP0109
MCSP0110
MCSP0111
MCSP0112
MCSP0199
MCSP0200
MCSP0201
MCSP0203

```



```

C      DC 23 I=1,N
      DO 23 J=1,N
      PHIS(I,J) = PHI(I,J)
      WRITE (6,131)
      CALL MWRITE (PHI,N,N)
C
C      CALL MREAD (H,M,N)
      DO 25 I=1,M
      DO 25 J=1,N
      HS(I,J) = H(I,J)
      WRITE (6,132)
      CALL MWRITE (H,M,N)
C
C      CALL MREAD (R,M,M)
      WRITE (6,133)
      CALL MWRITE (R,M,M)
C
C      CALL MREAD (COVW,IN,IN)
      WRITE (6,134)
      CALL MWRITE (COVW,IN,IN)
      CALL MREAD (GAMMA,N,IN)
C
C      DO 30 I=1,N
      DO 30 J=1,IN
      GAMMAS(I,J) = GAMMA(I,J)
      WRITE (6,136)
      CALL MWRITE (GAMMA,N,IN)
C
C      CALL MREAD (PKKM1,N,N)
      WRITE (6,137)
      CALL MWRITE (PKKM1,N,N)
C
C      DO 311 K=2,NR
      CALL MREAD (PRR,N,N)
      DO 310 I=1,N
      DO 310 J=1,N
      PR(I,J,K) = PRR(I,J)
      310 CONTINUE
C
C      CALL VREAD (SIGV,M)
      WRITE (6,138)

```

```

MCSP0204
MCSP0205
MCSP0207
MCSP0208
MCSP0210
MCSP0211
MCSP0212
MCSP0213
MCSP0215
MCSP0217
MCSP0219
MCSP0220
MCSP0222
MCSP0223
MCSP0224
MCSP0225
MCSP0227
MCSP0228
MCSP0229
MCSP0230
MCSP0231
MCSP0233
MCSP0234
MCSP0235
MCSP0244
MCSP0245
MCSP0246
MCSP0248
MCSP0249
MCSP0251
MCSP0252
MCSP0253
MCSP0254
MCSP0256
MCSP0257
MCSP0258
MCSP0259
CH3*****1
CH3*****2
CH3*****3
CH3*****4
CH3*****5
CH3*****6
MCSP0260
MCSP0262
MCSP0263

```

```

C      CALL VWRITE (SIGV,M)
C
C      DO 340 I=1,NR
C      READ (5,144) (XHATZ(I,J),J=1,N)
C      WRITE (6,140)
C      WRITE (6,146) (XHATZ(I,J),J=1,N)
C
C      340
C
C      36 DO 360 I=1,NR
C      READ (5,144) (XS(I,J,1),J=1,N)
C      INITIAL CONDITION HAS BEEN READ
C      WRITE (6,143)
C      WRITE (6,146) (XS(I,J,1),J=1,N)
C
C      360
C
C      38 CALL TRACK
C
C
C      DO 390 K=1,NR
C      WRITE (6,145)
C      WRITE (6,146) (XS(K,I,1),I=1,N)
C      WRITE (6,146) (XS(K,I,NSAM),I=1,N)
C      CCNTINUE
C
C      39
C      390
C
C      THE FOLLOWING SECTION PREPARES FOR THE MONTE CARLO LOOP
C      FORM NXN IDENTITY MATRIX IN DOUBLE PRECISION
C
C      DO 41 I=1,N
C      DO 41 J=1,N
C      EI(I,J) = 0.00
C      IF (I.EQ.J) EI(I,J)=1.00
C      41
C
C      GIVEN THE MATRIX GAMMA AND THE COVARIANCE OF W COMPUTE Q
C      USING DOUBLE PRECISION ARITHMETIC
C
C      CALL QMAY
C      WRITE (6,135)
C      CALL MWWRITE (Q,N,N)
C
C      SET UP ARRAYS FOR COMPUTING STATISTICS
C
C      DO 48 I=1,NR
C      DO 48 K=1,NSAM
C      DC 48 J=1,N

```

```

MCSP0264
MCSP0265
MCSP0272
CH200006
CH200007
MCSP0275
CH200008
MCSP0277
MCSP0292
CH200009
CH200010
MCSP0294
MCSP0295
CH200011
MCSP0302
MCSP0247
MCSP0304
MCSP0250
MCSP0307
CH200012
MCSP0308
CH200013
CH200014
CH200015
MCSP0313
MCSP0314
MCSP0221
MCSP0316
MCSP0317
MCSP0318
MCSP0320
MCSP0321
MCSP0322
MCSP0323
MCSP0324
MCSP0325
MCSP0319
MCSP0327
MCSP0328
MCSP0329
MCSP0356
MCSP0357
MCSP0358
CH200016
MCSP0359
MCSP0360
MCSP0361

```

```

C      XM(I,J,K) = 0.
C      ERR(I,J,K) = 0.
C      DO 48 L=1,N
C      48  VAR(J,L,K) = 0.
C
C      BEGIN MAIN ITERATION LOOP HERE
C      DC 54 ITER=1,NENS
C
C      49  DO 50 I=1,N
C      50  XHKKM1(I) = XHATZ(1,I)
C
C      DO 54 K=1,NSAM
C      FORM NOISY MEASUREMENT FROM TRUE STATE VALUE
C
C      DO 51 I=1,N
C      51  X(I) = XS(1,I,K)
C      CALL GAIN
C
C      DO 52 I=1,N
C      DO 52 J=1,M
C      52  GKS(I,J,K) = G(I,J)
C
C      UPDATE THE STATE ESTIMATE
C      53  CALL ESTIM
C      UPDATE RUNNING SUMS USED IN COMPUTING STATISTICS
C      CALL STAT
C
C      54  CCNTINUE
C
C      DIVIDE RUNNING SUMS COMPUTED BY SUBROUTINE STAT BY ENSEMBLE
C      SIZE TO COMPUTE STATISTICS
C      ENS = NENS
C      DO 56 K=1,NSAM
C      DO 56 J=1,N
C      55  ERR(1,J,K) = ERR(1,J,K)/ENS
C
C      CH200017
C      CH200019
C      MCSP0364
C      MCSP0365
C      MCSP0366
C      MCSP0367
C      MCSP0368
C      MCSP0369
C      MCSP0370
C      MCSP0371
C      MCSP0372
C      MCSP0375
C      MCSP0376
C      CH200018
C      MCSP0378
C      MCSP0379
C      MCSP0380
C      MCSP0381
C      MCSP0382
C      MCSP0383
C      MCSP0384
C      CH200020
C      MCSP0386
C      MCSP0396
C      MCSP0397
C      MCSP0398
C      MCSP0400
C      MCSP0401
C      MCSP0402
C      MCSP0403
C      MCSP0404
C      MCSP0405
C      MCSP0406
C      MCSP0407
C      MCSP0408
C      MCSP0409
C      MCSP0411
C      MCSP0414
C      MCSP0415
C      MCSP0416
C      MCSP0417
C      MCSP0418
C      MCSP0419
C      MCSP0420
C      MCSP0421
C      MCSP0422
C      MCSP0423
C      CH200022

```

```

C C C
56 VAR(J,J,K) = VAR(J,J,K)/ENS-ERR(1,J,K)**2
C
C
C
      IF (IPRT.NE.0) GO TO 64
      CALL PRT
      IF (IPLT.NE.0) GO TO 80
      CALL PLT
      CONTINUE
      STOP
C
81 FORMAT (6(I10))
82 FORMAT (12)
83 FORMAT (7(I10))
84 FORMAT (2(I5))
85 FORMAT (5(I10))
130 FORMAT (4X,N=,I2,4X,M=,I2,4X,IN=,I2,4X,NSAM=,I3,4X,NENS=,IMCSP0616
131 FORMAT (//,10X,THE PHI MATRIX IS,/)
132 FORMAT (//,10X,THE H MATRIX IS,/)
133 FORMAT (//,10X,THE H MATRIX IS,/)
134 FORMAT (//,10X,THE COVARIANCE OF W MATRIX IS,/)
135 FORMAT (//,10X,THE Q MATRIX IS,/)
136 FORMAT (//,10X,THE GAMMA MATRIX IS,/)
137 FORMAT (//,10X,THE GAMMA P(0/-1) IS,/)
138 FORMAT (//,10X,THE STD. DEVIATIONS OF MEASUREMENT NOISE ARE,/)
139 FORMAT (//,10X,THE STD. DEVIATIONS OF INPUT FORCING W ARE,/)
140 FORMAT (//,10X,THE VECTOR XHAT(0/-1) IS,/)
141 FORMAT (//,10X,THE MEAN OF THE VECTOR X(0) IS,/)
142 FORMAT (//,10X,THE STANDARD DEVIATIONS OF THE VECTOR X(0) ARE,/)
143 FORMAT (//,10X,THE INITIAL STATE IS,/)
144 FORMAT (//,10X,THE FIRST AND LAST POINTS ON THE SINGLE TRACK TO BMCSP0630
145 IE USED ARE,/)
146 FORMAT (9(2X,1PE12.5),/)
150 END
C
C
C
      SLBRoutine QMAT
      THIS SUBROUTINE COMPUTES THE MATRIX Q FROM THE EQUATION
      Q=GAMMA* E(W*WT) * GAMMAT
      DCUBLE PRECISION ARITHMETIC IS USED
C
C
C
      MCSP0428
      MCSP0444
      MCSP0445
      MCSP0489
      MCSP0490
      MCSP0552
      MCSP0553
      MCSP0554
      CH200024
      MCSP0556
      MCSP0557
      MCSP0558
      MCSP0616
      MCSP0617
      MCSP0618
      MCSP0619
      MCSP0620
      MCSP0621
      MCSP0622
      MCSP0623
      MCSP0624
      MCSP0625
      MCSP0626
      MCSP0627
      MCSP0628
      MCSP0629
      MCSP0630
      MCSP0631
      MCSP0632
      MCSP0633
      MCSP0654
      MCSP0399
      MCSP0764
      MCSP0765
      MCSP0766
      MCSP0767
      MCSP0768
      MCSP0769
      MCSP0770
      MCSP0771

```



```

C
REAL*8 GAMMA,COVW,R,PHI,H,TEMP,TEMP1,TEMP2,PKKM1,G,PKK,Q,EI,PR
COMMON EI(4,4),Q(4,4),G(4,4),PKK(4,4),GAMMA(4,4),COVW(4,4),
1TEMP(4,4),TEMP1(4,4),TEMP2(4,4),H(4,4),PKKM1(4,4),R(4,4),PHI(4,4),
2VAR(4,4,60),GKS(4,4,60),PKKS(4,4,60),XM(4,4,60),ERR(4,4,60),
3GAMMAS(4,4),PHIS(4,4),XS(4,4,60),HS(4,4),GK(4,4),SIGW(4),X(4),
4SIGXZ(4),XZMEAN(4),XHKK(4),XHKKMI(4),VTMP(4),Z(4),V(4),SIGV(4),
5XHATZ(4,4),YZ(60),PX(10),PY(10),PR(4,4,4),
6N,NSAM,IQ,M,ITER,ITRK,IN,ISTAT,K,ITRO,IXZ,IV,IW,TEST,ND,NR
MCSP0772
CH3*****
MCSP0774
MCSP0775
CH200025
CH200026
MCSP0778
CH200004
CH2
MCSP0781
MCSP0782
MCSP0783
MCSP0784
MCSP0785
MCSP0786
MCSP0787
MCSP0788
MCSP0789
MCSP0790
MCSP0791
MCSP0792
CH3*****
MCSP0794
MCSP0795
CH200028
CH200029
MCSP0798
CH200004
CH2
MCSP0801
MCSP0802
MCSP0803
MCSP0804
MCSP0805
MCSP0806
MCSP0807
MCSP0808
MCSP0809
MCSP0810
MCSP0811
CH3*****
MCSP0813
MCSP0814
CH200031
CH200032
MCSP0817
CH200004
CH2

```

```

C
CALL PROD (GAMMA,COVW,N,IN,IN,TEMP)
CALL TRANS (GAMMA,N,IN,TEMP1)
CALL PROD (TEMP,TEMP1,N,IN,N,Q)
RETURN
END
SUBROUTINE QON

```

```

C
IF Q IS TO BE COMPUTED ON-LINE (IFLQ.NE.0) IT IS DONE
IN THIS SUBROUTINE

```

```

C
REAL*8 GAMMA,COVW,R,PHI,H,TEMP,TEMP1,TEMP2,PKKM1,G,PKK,Q,EI,PR
COMMON EI(4,4),Q(4,4),G(4,4),PKK(4,4),GAMMA(4,4),COVW(4,4),
1TEMP(4,4),TEMP1(4,4),TEMP2(4,4),H(4,4),PKKM1(4,4),R(4,4),PHI(4,4),
2VAR(4,4,60),GKS(4,4,60),PKKS(4,4,60),XM(4,4,60),ERR(4,4,60),
3GAMMAS(4,4),PHIS(4,4),XS(4,4,60),HS(4,4),GK(4,4),SIGW(4),X(4),
4SIGXZ(4),XZMEAN(4),XHKK(4),XHKKMI(4),VTMP(4),Z(4),V(4),SIGV(4),
5XHATZ(4,4),YZ(60),PX(10),PY(10),PR(4,4,4),
6N,NSAM,IQ,M,ITER,ITRK,IN,ISTAT,K,ITRO,IXZ,IV,IW,TEST,ND,NR

```

```

C
THE APPROPRIATE STATEMENTS FOR COMPUTING Q ON-LINE MUST
BE INSERTED HERE BY THE USER
RETURN
END
SUBROUTINE RON

```

```

C
IF R IS TO BE COMPUTED ON-LINE (IFLR.NE.0) IT IS DONE
IN THIS SUBROUTINE

```

```

C
REAL*8 GAMMA,COVW,R,PHI,H,TEMP,TEMP1,TEMP2,PKKM1,G,PKK,Q,EI,PR
COMMON EI(4,4),Q(4,4),G(4,4),PKK(4,4),GAMMA(4,4),COVW(4,4),
1TEMP(4,4),TEMP1(4,4),TEMP2(4,4),H(4,4),PKKM1(4,4),R(4,4),PHI(4,4),
2VAR(4,4,60),GKS(4,4,60),PKKS(4,4,60),XM(4,4,60),ERR(4,4,60),
3GAMMAS(4,4),PHIS(4,4),XS(4,4,60),HS(4,4),GK(4,4),SIGW(4),X(4),
4SIGXZ(4),XZMEAN(4),XHKK(4),XHKKMI(4),VTMP(4),Z(4),V(4),SIGV(4),
5XHATZ(4,4),YZ(60),PX(10),PY(10),PR(4,4,4),
6N,NSAM,IQ,M,ITER,ITRK,IN,ISTAT,K,ITRO,IXZ,IV,IW,TEST,ND,NR

```


MC SP08666
MC SP08667
MC SP08668
MC SP08669
MC SP08670
MC SP09334
MC SP09335
MC SP09336
MC SP09337
CH3**09337
MC SP09339
MC SP09340
CH2000401
CH2000411
MC SP09433
CH2
MC200000*
MC SP09466
MC SP09477
MC SP09498
CH2
MC SP09501
MC SP09510
MC SP09512
MC SP09513
MC SP09514
MC SP09515
MC SP09516
MC SP09517
MC SP09518
MC SP09519
MC SP09559
MC SP09601
MC SP09611
MC SP09623
MC SP09633
MC SP09644
MC SP09655
MC SP09666
MC SP09667
MC SP09677
MC SP09699
MC SP09701
MC SP09711
MC SP09712
MC SP09713
MC SP09714
MC SP09715
MC SP09716

```

C      2 FORMAT (8F10.0)
C      END
C      SUBROUTINE MWRITE (A,N,M)
C      THIS SUBROUTINE WRITES THE ENTRIES OF THE NXM MATRIX A
C      REAL*8 A
C      DIMENSION A(4,4)
C
C      DC 1 I=1,N
C      1 WRITE (6,2) (A(I,J),J=1,M)
C
C      RETURN
C
C      2 FORMAT (9(2X,1PE12.5))
C      END
C      SUBROUTINE PROD (A,B,N,M,L,C)
C      THIS SUBROUTINE COMPUTES THE MATRIX PRODUCT AB AND STORES THE
C      RESULT IN C
C      A = NXM, B = MXL, C = NXL
C      REAL*8 A,B,C,T
C      DIMENSION A(4,4),B(4,4),C(4,4),T(4,4)
C
C      DC 1 I=1,N
C
C      DO 1 J=1,L
C      1 T(I,J) = 0.0
C
C      DC 2 I=1,N
C      DC 2 J=1,L
C
C      DO 2 K=1,M
C      2 T(I,J) = T(I,J)+A(I,K)*B(K,J)
C
C      DO 3 I=1,N
C      DC 3 J=1,L
C      3 C(I,J) = T(I,J)
C
C      RETURN
C      END
C      SUBROUTINE SUB (A,B,N,M,C)
C      THIS SUBROUTINE SUBTRACTS THE NXM MATRIX B FROM THE NXM MATRIX
C      A AND STORES THE RESULT IN C
C      REAL*8 A,B,C
C      DIMENSION A(4,4),B(4,4),C(4,4)

```

MCSP0977
 MCSP0978
 MCSP0979
 MCSP0980
 MCSP0981
 MCSP0982
 MCSP0983
 MCSP0984
 MCSP0985
 MCSP0986
 MCSP0987
 MCSP0988
 MCSP0989
 MCSP0990
 MCSP0991
 MCSP0992
 MCSP0993
 MCSP0994
 MCSP0995
 MCSP0996
 MCSP0997
 MCSP0998
 MCSP0999
 MCSP1000
 MCSP1001
 MCSP1002
 MCSP1003
 MCSP1004
 MCSP1005
 MCSP1006
 MCSP1007
 MCSP1008
 MCSP1009
 MCSP1010
 MCSP1011
 MCSP1012
 MCSP1013
 MCSP1014
 MCSP1015
 MCSP1016
 MCSP1017
 MCSP1018
 MCSP1019
 MCSP1020
 MCSP1021
 MCSP1022
 MCSP1023
 MCSP1024

```

C      DC 1 I=1,N
C      DC 1 J=1,M
C      1 C(I,J) = A(I,J)-B(I,J)
C      RETURN
C      END
C      SUBROUTINE TRANS (A,N,M,C)
C      THIS SUBROUTINE FORMS THE MATRIX TRANSPOSE OF A STORING THE
C      RESULT IN C
C      A = NXM, C = MXN
C      REAL*8 A,C
C      DIMENSION A(4,4),C(4,4)
C      DO 1 I=1,N
C      DC 1 J=1,M
C      1 C(J,I) = A(I,J)
C      RETURN
C      END
C      SUBROUTINE VADD (X,Y,N,Z)
C      THIS SUBROUTINE COMPUTES THE SUM OF THE N-VECTORS X AND
C      Y AND STORES THE RESULT IN THE N-VECTOR Z
C      REAL*4 X(4),Y(4),Z(4)
C      DC 1 I=1,N
C      1 Z(I) = X(I)+Y(I)
C      RETURN
C      END
C      SUBROUTINE VPROD (A,X,M,N,Y)
C      THIS SUBROUTINE COMPUTES THE PRODUCT OF THE MXN MATRIX
C      A AND THE N-VECTOR X AND STORES THE RESULT IN THE
C      M-VECTOR Y
C      REAL*4 A(4,4),X(4),Y(4),T(4)
C      DO 1 I=1,M
C      T(I) = 0.00
C      DO 1 J=1,N
C      1 T(I) = T(I)+A(I,J)*X(J)
C      C
C

```

MCSPI025
 MCSPI026
 MCSPI027
 MCSPI028
 MCSPI029
 MCSPI030
 MCSPI031
 MCSPI032
 MCSPI033
 MCSPI034
 MCSPI035
 MCSPI036
 MCSPI037
 MCSPI038
 MCSPI039
 MCSPI040
 MCSPI041
 MCSPI042
 MCSPI043
 MCSPI044
 MCSPI045
 MCSPI046
 MCSPI047
 MCSPI048
 MCSPI049
 MCSPI050
 MCSPI051
 MCSPI052
 MCSPI053
 MCSPI054
 MCSPI055
 MCSPI056
 MCSPI057
 MCSPI058
 MCSPI059
 MCSPI060
 MCSPI061
 MCSPI062
 MCSPI063
 MCSPI064
 MCSPI065
 MCSPI066
 MCSPI067
 MCSPI068
 MCSPI069
 MCSPI070
 MCSPI071
 MCSPI072


```

TPI = 2.*3.14159265
DC 5 K=2,NSAM
EKM1 = K-1
T = 1.0*EKM1
A=0.033333*T
IF(A.LT.TPI) GO TO 10
FM=MM
A = A - FM*TPI
10 CCNTINUE
XS(1,1,K)=10.*SIN(A)
XS(1,2,K)=.3333*COS(A)
XS(1,3,K)=10.*COS(A)
XS(1,4,K)=-.3333*SIN(A)
DO 7 I=2,NR
EKM1 = K-1
XS(I,1,K) = XS(I,1,EKM1) + XS(I,2,1)
XS(I,2,K) = XS(I,2,1)
XS(I,3,K) = XS(I,3,EKM1) + XS(I,4,1)
XS(I,4,K) = XS(I,4,1)
7 CCNTINUE
5
END
SUBROUTINE MEAS
THIS SUBROUTINE STARTS WITH THE TRUE STATE VALUE XS
AND ADDS ZERO-MEAN WHITE GAUSSIAN NOISE TO H*XS TO
GENERATE A NOISY VECTOR OF MEASUREMENTS Z.
C
C
C
C
REAL*8 GAMMA,COVW,R,PHI,H,TEMP,TEMP1,TEMP2,PKKM1,G,PKK,Q,EI,PR
COMMON EI(4,4),Q(4,4),G(4,4),PKK(4,4),GAMMA(4,4),COVW(4,4),
1TEMP(4,4),TEMP1(4,4),TEMP2(4,4),H(4,4),PKKM1(4,4),PHI(4,4),
2VAR(4,4,60),GKS(4,4,60),PKKS(4,4,60),XM(4,4,60),ERR(4,4,60),
3GAMMAS(4,4),PHIS(4,4),XS(4,4,60),HS(4,4),GK(4,4),SIGW(4,4),
4SIGXZ(4,4),XZMEAN(4,4),XHKK(4,4),XHKKM1(4,4),VTMP(4,4),Z(4,4),
5XHAIZ(4,4),XZ(60),YZ(60),PX(10),PY(10),PR(4,4,4),
6N,NSAM,IQ,M,ITER,I TRK,IN,ISTAT,K,ITRO,IXZ,IV,IW,IEST,ND,NR
ALPHA = XS(1,3,K)
BETA = XS(1,1,K)
Z(1) = SQRT(ALPHA**2+BETA**2)
Z(2) = ATAN2(ALPHA,BETA)
CALL SNORM (IV,V,M)
C
DC 1 I=1,M
1 V(I) = SIGV(I)*V(I)
C
CALL VADD (Z,V,M,Z)

```

MCSP0918
MCSP0919

CH200046
CH200047
CH200048
CH200049
CH200050
CH200051
CH200053
CH200054
CH200055
CH200056
CH200057
MCSP0925
MCSP0926
MCSP0933
MCSP0734
MCSP0735
MCSP0736
MCSP0737
MCSP0738
MCSP0739
CH3****
MCSP0741
MCSP0742
CH200058
CH200059
MCSP0745
CH200000*
CH2
CH200061
CH200062
MCSP0750
MCSP0751
MCSP0752
MCSP0753
MCSP0754
MCSP0755
MCSP0756
MCSP0757

```

C      ALPHA = Z(1)*COS(Z(2))
C      BETA = Z(1)*SIN(Z(2))
C      XZ(K)=ALPHA
C      YZ(K)=BETA
C      RETURN
C      END
C
C      SLROUTINE GAIN
C
C      REAL*8 GAMMA, COVM, R, PHI, H, TEMP, TEMPI, TEMP2, PKKM1, G, PKK, Q, EI, PR
C      COMMON EI(4,4), Q(4,4), G(4,4), PKK(4,4), GAMMA(4,4), COVM(4,4), PHI(4,4), PR
C      1TEMP(4,4), TEMPI(4,4), TEMP2(4,4), H(4,4), PKKM1(4,4), R(4,4), ERR(4,4), X(4,4),
C      2VAR(4,4,60), GKS(4,4,60), PKKS(4,4,60), XM(4,4,60), GK(4,4,60), SIGW(4,4), X(4,4),
C      3GAMMAS(4,4), PHIS(4,4), XS(4,4,60), HS(4,4,60), V(4,4), SIGV(4,4),
C      4SIGXZ(4,4), XZMEAN(4,4), XHKK(4,4), XHKKM1(4,4), VTMP(4,4), Z(4,4),
C      5XHATZ(4,4), XZ(60), YZ(60), PX(10), PY(10), PR(4,4,4),
C      6NSAM, IQ, M, ITER, ITRK, IN, ISTAT, K, ITRO, IXZ, IV, IW, IEST, ND, NR
C      DIMENSION BE(4), ER(4)
C
C      G(K) = P(K/K-1)*HT*(H*P(K/K-1)*HT + R)
C      DC 300 I=1,4
C      DO 300 J=1,4
C      300 PKKS(I,J,K)=PKKM1(I,J)
C
C      IF(DABS(PKKM1(1,1)-PKKM1(3,3)).GT.0) GO TO 11
C      PKKM1(1,1)=PKKM1(3,3)+0.000001
C      11 CONTINUE
C
C      FINE UPDATE UNIT'S ELLIPSE ORIENTATION
C
C      THE=0.5*DATAN(2.*PKKM1(1,3)/(PKKM1(1,1)-PKKM1(3,3)))
C      IF(ABS(THET).GT.0) GO TO 10
C      TFE = 0.00001
C      10 CONTINUE
C
C      FINE UNCOUPLED VARIANCES
C
C      SIG2X=(PKKM1(1,1)+PKKM1(3,3))/2.+PKKM1(1,3)/SIN(2.*THE)
C      SIG2Y=(PKKM1(1,1)+PKKM1(3,3))/2.-PKKM1(1,3)/SIN(2.*THE)
C
C      ADJUST THETA
C
C      IF(SIG2X.GE.SIG2Y) GO TO 63
C      TFE=THE+.34159265/2.
C
C      CALCULATE BEARING
C
C      DC 9 IN=1,3

```



```

CH3?????
CH3?????
CH3***12

PLR06430
PLR06440
PLR06450
PLR06460
PLR06470
PLR06480
PLR06490

SIG2YR = - SIG2YR
21 CONTINUE
ERP = BE(IN) - THER

CIND THE MAJOR AND MINOR AXES
IF(SIG2XR-GE.SIG2YR)GO TO 24
SIGMJ = SIG2YR
SIGMN = SIG2XR
GO TO 25
24 SIGMJ = SIG2XR
SIGMN = SIG2YR
25 CCNTINUE

CALCULATE THE NOISE COVARIANCE
R(1,1) = SIGMJ*SIGMN/ SIGMJ*[(SIN(ERP))**2] + SIGMN*((COS(ERP))**2PLR06500
WRITE (6,23)
23 FCRMAT (6X,'THER',12X,'SIG2XR', 8X,'SIG2YR', 9X,'ERP',10X,'R(1,1)',CH3*****
1,10X,'BE(3,1)')
CALL TRANS (H,M,N,TEMP2)
CALL PROD (PKKM1,TEMP2,N,N,M,TEMP)
CALL PROD (H,TEMP,M,N,M,TEMP1)
CALL ADD (TEMP1,R,M,M,TEMP1)
IF (M.EQ.1) GO TO 2
MD = ND
CALL GAUSS3 (M,EPS,TEMP1,TEMP2,KER,MD)
CALL PROD (TEMP,TEMP2,N,M,M,G)

NOTE HERE PKK(I,J) = P(K/K) WHERE
P(K/K) = (I-G(K)*H)*P(K/K-1)
1 CALL PROD (G,H,N,M,N,TEMP)
CALL SUB (EI,TEMP,N,N,TEMP2)
CALL PROD (TEMP2,PKKM1,N,N,N,PKK)

NOTE HERE PKKM1(I,J) = P(K/K-1) WHERE
P(K/K-1) = PHI*P(K-1/K-1)*PHIT + Q
CALL TRANS (PHI,N,N,TEMP2)
CALL PROD (PKK,TEMP2,N,N,N,TEMP)
CALL PROD (PHI,TEMP,N,N,N,TEMP1)
CALL ADD (TEMP1,Q,N,N,PKKM1)
RETURN

2 DO 3 I=1,N
3 G(I,1) = TEMP(I,1)/TEMP1(1,1)
GO TO 1

```



```

154 FORMAT (6X, I3, I3X, I1, I0X, IPE14.7, 2(6X, IPE14.7))
155 FORMAT (//)
156 FCRMAT (.1)
157 FCRMAT (I0X, 'THE SAMPLE COVARIANCE OF EST. ERROR MATRIX IS', //)
158 FCRMAT (//, 2X, 'K=', I3, /)
      RETURN
      END
      SUBROUTINE PLT
      REAL*8 GAMMA, COVW, R, PHI, H, TEMP, TEMP1, TEMP2, PKKM1, G, PKK, Q, EI, PR
      COMMON EI(4,4), Q(4,4), G(4,4), PKK(4,4), GAMMA(4,4), COVW(4,4), PHI(4,4), PR
      1TEMP(4,4), TEMP1(4,4), H(4,4), PKKM1(4,4), R(4,4), ERR(4,4), X(4,4),
      2VAR(4,4,60), GK(4,4,60), PKKS(4,4,60), XM(4,4,60), ER(4,4,60),
      3GAMMAS(4,4), PHIS(4,4), XS(4,4,60), HS(4,4), GK(4,4), SIGW(4,4), X(4,4),
      4SIGXZ(4,4), XZMEAN(4,4), XHKK(4,4), XHKKM1(4,4), VTM(4,4), V(4,4), SIGV(4,4),
      5XHATZ(4,4), XZ(60), YZ(60), PX(10), PY(10), PR(4,4,4), IEST, ND, NR
      6N, NSAM, IQ, M, ITER, ITRK, IN, ISTAT, K, ITRO, IXZ, IV, IW, IEST, ND, NR
      INTEGER*4 ITB(12)/12*0/
      REAL*4 RTB(28)/28*0.0/
      DIMENSION XP(60), YP(60)
      EQUIVALENCE (TITLE, RTB(5))
      REAL*8 TITLE(12)/X = TRUE, + = FILTER, SQUARE = NOISY*/

      IGPLT=1
      ITHVPL=1
      IHTPLT=1
      ISMPLT=1
      ISVPLT=1
      DO 500 KY=1, NR
      KX=NR+1-KY
      DO 50 K=1, NSAM
      XP(K) = XM(KX, 1, K)
      YP(K) = XM(KX, 3, K)
      50 CALL PLOTTP(XP, YP, NSAM, 0)
      500 CONTINUE
      ITB(1)=1
      ITB(2)=1
      CALL DRAWP(60, XP, YP, ITB, RTB)
      DO 51 K=1, NSAM
      XP(K)=XS(1, 1, K)+ERR(1, 1, K)
      YP(K)=XS(1, 3, K)+ERR(1, 3, K)
      51 CALL PLOTTP(XP, YP, NSAM, 0)
      ITB(1)=2
      ITB(2)=2
      CALL DRAWP(60, XP, YP, ITB, RTB)
      ITB(2)=0
      DO 2 J=1, 60, 5
      IF (ABS(PKKS(1, 1, J)-PKKS(3, 3, J)).GT.0) GO TO 11

```

MCSP0644
MCSP0645
MCSP0646
MCSP0647
MCSP0648

CH3*****
MCSP0879
MCSP0880
CH200083
CH200084
MCSP0883
CH200000*
CH2

CH2*****
CH2*****
CH2*****
CH2*****
CH2*****

CH200088
CH200089

```

11 CONTINUE
   THE=0.5*ATAN(2.*PKKS(1,3,J)/(PKKS(1,1,J)-PKKS(3,3,J)))
   IF (ABS(THE).GT.0) GO TO 10
   THE=0.000001
10 CONTINUE
   SIG2X=(PKKS(1,1,J)+PKKS(3,3,J))/2.+PKKS(1,3,J)/SIN(2.*THE)
   WRITE(6,146) THE, SIG2X, SIG2Y
146 FORMAT (9(2X,1PE12.5),/)
   SX=(SIG2X)**.5*20.
   SY=(SIG2Y)**.5*20.
   PT=3.14159265/12.
   CT=COS( THE )
   ST=SIN( THE )
   DO 1 I=1,25
     XI=I
     XP(I)=SX*COS(PT*XI)*CT-SY*SIN(PT*XI)*ST+XS(1,1,J)
     YP(I)=SX*COS(PT*XI)*ST+SY*SIN(PT*XI)*CT+XS(1,3,J)
     DO 201 J=2, NR
       DO 200 K=1, NSAM
         XP(K)=XS(J,1,K)
         YP(K)=XS(J,3,K)
         IT=(J/2)+3
         ITB(2)=IT
         CALL DRAWP (60,XP,YP,ITB,RTB)
200   ITB(1)=3
         ITE(2)=3
         CALL DRAWP (60,XZ,YZ,ITB,RTB)
         DO 65 K=1, NSAM
           XP(K) = K
65   IF (IGPLT.NE.1) GO TO 68
C
C   DO 67 I=1,N
C
C   DO 67 J=1,M
C
C   DO 66 K=1, NSAM
66   YP(K) = GKS(I,J,K)
C
C   WRITE (6,156)
   CALL PLOT (XP,YP,NSAM,0)
67   WRITE (6,159) I,J
C
68   IF (ITHVPL.NE.1) GO TO 71
C

```

CH2000090
CH2000091
CH2000092
CH2000093
CH2000094
CH2000095
CH2000096
CH2000097
CH2000098

MCSP0491
MCSP0492
MCSP0493
MCSP0494
MCSP0495
MCSP0496
MCSP0497
MCSP0498
MCSP0499
MCSP0500
MCSP0501
MCSP0502
MCSP0503
MCSP0504
MCSP0505
MCSP0506
MCSP0507
MCSP0508

```

C      DO 70 I=1,N
C      DO 69 K=1,NSAM
C      69 YP(K) = PKKS(I,I,K)
C      WRITE (6,156)
C      CALL PLOTP (XP,YP,NSAM,0)
C      70 WRITE (6,160) I,I
C      71 IF (IMTPLT.NE.1) GO TO 74
C      DO 73 I=1,N
C      DO 72 K=1,NSAM
C      72 YP(K) = XM(I,I,K)
C      WRITE (6,156)
C      CALL PLOTP (XP,YP,NSAM,0)
C      73 WRITE (6,161) I
C      74 IF (ISMPLT.NE.1) GO TO 77
C      DO 76 I=1,N
C      DO 75 K=1,NSAM
C      75 YP(K) = ERR(I,I,K)
C      WRITE (6,156)
C      CALL PLOTP (XP,YP,NSAM,0)
C      76 WRITE (6,162) I,I
C      77 IF (ISVPLT.NE.1) GO TO 80
C      DO 79 I=1,N
C      DO 78 K=1,NSAM
C      78 YP(K) = VAR(I,I,K)
C      WRITE (6,156)
C      CALL PLOTP (XP,YP,NSAM,0)
C      79 WRITE (6,163) I
C      80 CONTINUE
C      WRITE (6,156)
C      156 FORMAT (11,1)
C      159 FORMAT (12X,'G(,11,,11,,) VS. K,')
C      160 FORMAT (12X,'PKK(,11,,11,,) VS. K,')
C      161 FORMAT (12X,'MEAN OF X(,11,,) VS. K,')

```

```

MCSP0509
MCSP0510
MCSP0511
MCSP0512
MCSP0513
MCSP0514
MCSP0515
MCSP0516
MCSP0517
MCSP0518
MCSP0519
MCSP0520
MCSP0521
MCSP0522
CH200099
MCSP0524
MCSP0525
MCSP0526
MCSP0527
MCSP0528
MCSP0529
MCSP0530
MCSP0531
MCSP0532
MCSP0533
CH2
MCSP0535
MCSP0536
MCSP0537
MCSP0538
MCSP0539
MCSP0540
MCSP0541
MCSP0542
MCSP0543
MCSP0544
MCSP0545
MCSP0546
MCSP0547
MCSP0548
MCSP0549
MCSP0550
MCSP0551
MCSP0649
MCSP0650
MCSP0651

```


MCSP0652
MCSP0653

162 FORMAT (12X,'XHATKK(',I1,',') -X(',I1,',') VS. K')
163 FORMAT (12X,'ERROR VARIANCE(',I1,',') VS.. K')
RETURN
END

//GO.FT06F001 DD SYSOUT=A,SPACE=(CYL,(4,1))

//GO.SYSIN DD *

\$\$\$\$\$\$\$\$\$DATA DECK\$\$\$\$\$\$\$\$\$

ND	N	M	IN	NSAM	NENS	NR
4	4	1	2	60	1	4

IPRT IPLT

1.0 1.0 1.0 1.0

PHI

H

1.0

R

0.0001

COVM

0.0001

0.0001

GAMMA

0.5

1.0

PKKM1

0.0001

0.0001

PRR(1)

0.0001

0.0001

PRR(2)

0.0001

0.0001

PRR(3)

0.0001

[illegible]

LIST OF REFERENCES

1. Dittmar, C. A. , Jr., The Application of Extended Kalman Filtering to the Position Locating Reporting System (PLRS), MSEE Thesis, Naval Postgraduate School, Monterey, California, 1975.
2. Sorenson, H. W., "Kalman Filtering Techniques," Advanced Control System, Vol. 3, Chapter 5, 1966.

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